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$$U(s) = \frac{\tau s + 1}{K(\tau_c s + 1 - e^{-\tau_D s})} E(s)$$

$$U(s) K(\tau_c s + 1 - e^{-\tau_D s}) = (\tau s + 1) E(s)$$

$$\frac{K\tau_c s}{\tau s + 1}U(s) = E(s) - \frac{K}{\tau s + 1}U(s) + \frac{Ke^{-\tau_D s}}{\tau s + 1}U(s)$$

$$\frac{\kappa \tau_{c} s}{\tau_{s+1}} U(s) = E(s) - (G_M^* - G_M) U(s),$$

where  $G_M^*$  is the model of the process without the delay term

$$U(s) = \frac{\tau s + 1}{K \tau_c s} \left( E(s) - (G_M^* - G_M) U(s) \right)$$

- $\frac{\tau s+1}{K\tau_c s}$  represents a PI controller of the form  $\frac{\tau}{K\tau_c} \left(1+\frac{1}{\tau s}\right)$  where the gain of the controller is  $\frac{\tau}{K\tau_c}$  and the integral constant is  $\tau$
- The error term E(s) is corrected as  $\left(E(s)-(G_M^*-G_M)U(s)\right)$  using the model information





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$$U(s) = C(s) E(s)$$

$$V(s) = C(s) E(s)$$







#### Controller design for time delay systems - analysis of model information

Model information is used in the controller calculations

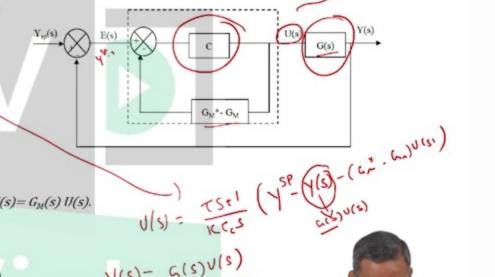
$$Y^{\text{des}} = \underbrace{\frac{e^{-\tau_D s}}{\tau_C s + 1}}$$

(4) (b) (C) (G) (Q) (---)

$$U(s) = \frac{\tau s + 1}{K \tau_c s} \left( E(s) - (G_M^* - G_M) U(s) \right)$$

If the model is perfect, then  $G(s)=G_M(s)$  and  $Y(s)=G(s)U(s)=G_M(s)$  U(s).

$$\begin{split} U(s) &= \frac{\tau s + 1}{K \tau_c s} \Big( Y_{sp}(s) - Y(s) - (G_M^* - G_M) U(s) \Big) \\ &= \frac{\tau s + 1}{K \tau_c s} \Big( Y_{sp}(s) - G_M(s) U(s) - (G_M^* - G_M) U(s) \Big) \\ &= \frac{\tau s + 1}{K \tau_c s} \Big( Y_{sp}(s) - G_M^*(s) U(s) \Big) \end{split}$$







### Controller design for time delay systems - analysis of model information

Model information is used in the controller calculations

$$Y^{\text{des}} = \underbrace{e^{-\tau_D s}}_{Cs+1}$$

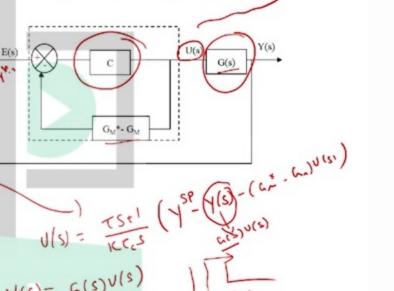
$$U(s) = \frac{\tau s + 1}{K \tau_c s} \left( E(s) - (G_M^* - G_M) U(s) \right)$$

If the model is perfect, then  $G(s)=G_M(s)$  and  $Y(s)=G(s)U(s)=G_M(s)$  U(s).

$$U(s) = \frac{\tau s + 1}{K \tau_c s} \left( Y_{sp}(s) - Y(s) - (G_M^* - G_M) U(s) \right)$$

$$= \frac{\tau s + 1}{K\tau_c s} \left( Y_{sp}(s) - G_M(s)U(s) - (G_M^* - G_M)U(s) \right)$$

$$\frac{\tau s + 1}{K\tau_c s} \left( Y_{sp}(s) - G_M^*(s)U(s) \right)$$



Y(s)= G(s)V(s) = Gn(s)V(s)



#### Vizle ansfer function inversion without approximation – another interpretation

Consider controller TF between the input and the error

$$U(s) = \underbrace{\frac{\tau s + 1}{K(\tau_c s + 1) - e^{-\tau_D s}}}_{K(\tau_c s + 1)} E(s)$$

$$\underbrace{\frac{K(\tau_c s + 1)}{\tau s + 1}}_{U(s)} U(s) = E(s) + \underbrace{\frac{Ke^{-\tau_D s}}{\tau s + 1}}_{U(s)} U(s)$$

$$\underbrace{\frac{\tau s + 1}{K(\tau_c s + 1)}}_{U(s)} E(s) + \underbrace{\frac{e^{-\tau_D s}}{(\tau_c s + 1)}}_{U(s)} U(s)$$

Let  $e^{-\tau_D s}$  be denoted as  $U^d(s)$ 

$$U(s) = \frac{\tau s + 1}{K(\tau_c s + 1)} E(s) + \frac{1}{(\tau_c s + 1)} U^d(s)$$

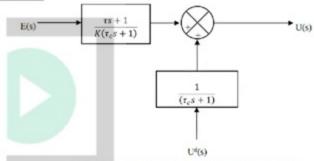
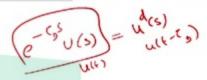


Fig: Inverting TF with time delay without approximation







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